Company

Address City, State Phone JOB TITLE Example 3.3 & 4.1

 JOB NO.
 SHEET NO.

 CALCULATED BY
 DATE

 CHECKED BY
 DATE

CS2024 Ver 2024-03-08

www.struware.com

# STRUCTURAL CALCULATIONS

## FOR

# 20' Eave Height using MWFRS all heights procedure 20' Eave Height using MWFRS <60' procedure

Guide to Wind Load Procedures ASCE 7-22

Company

Example 3.3 & 4.1 Example 3.3 & 4.1

Address City, State Phone

JOB NO. SHEET NO. \_\_\_\_\_ CALCULATED BY DATE \_\_\_\_\_ CHECKED BY DATE \_\_\_\_\_

www.struware.com

# Code Search

**Code:** ASCE 7 - 22

## **Occupancy:**

Occupancy Group = B Business

## **Risk Category & Importance Factors:**

Risk Category =	II
Wind Factor =	1.00
Snow Factor	1.00
Seismic Importance factor =	1.00

## **Type of Construction:**

Fire Rating:

Roof =	0.0 hr
Floor =	0.0 hr

## **Building Geometry:**

Roof angle (θ)	4.00 / 12	18.4 deg
Building length	250.0 ft	
Least width	200.0 ft	
Mean Roof Ht (h)	36.7 ft	
Parapet ht above grd	0.0 ft	
Minimum parapet ht	0.0 ft	
hb for Elevated bldg	0.0 ft	

#### Live Loads:

<u>Roof</u>	0 to 200 sf:	20 psf
	200 to 600 sf:	24 - 0.02Area, but not less than 12 psf
	over 600 sf:	12 psf

### Floor:

Typical Floor	100 psf
Partitions	N/A

## Company Address

Address		
City, State	JOB NO.	SHEET NO.
Phone	CALCULATED BY	DATE
	CHECKED BY	DATE

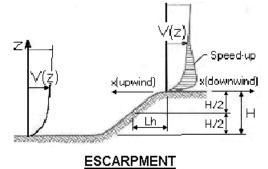
# Wind Loads :

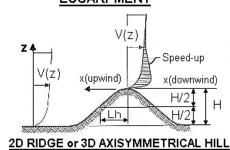
ASCE 7- 22
------------

Ultimate Wind Speed	115 mph
Nominal Wind Speed	89.1 mph
Risk Category	. II
Exposure Category	С
Enclosure Classif.	Enclosed Building
Internal pressure	+/-0.18
Bldg Directionality (Kd)	0.85
Kh MWFRS<=60	1.022
Kh all other	1.022
Type of roof	Gable

Topographic Fa	ctor (Kzt)		
Topography		Flat	
Hill Height	(H)	80.0 ft	
Half Hill Length	(Lh)	100.0 ft	
Actual H/Lh	=	0.80	
Use H/Lh	=	0.50	
Modified Lh	=	160.0 ft	
From top of cres	st: x =	50.0 ft	
Bldg up/down w	ind?	downwind	
H/Lh= 0.50		$K_1 = C$	000.
x/Lh = 0.31		$K_2 = 0$	.792
z/Lh = 0.23		K <sub>3</sub> = 1	.000
At Mean Roof H	t:		

$$Kzt = (1+K_1K_2K_3)^2 = 1.00$$





Gust Effect	Factor
h =	36.7 ft
B =	200.0 ft
/z (0.6h) =	22.0 ft

Rigid	Structure
ē =	0.20
ł =	500 ft
z <sub>min</sub> =	15 ft
c =	0.20
$g_Q, g_v =$	3.4
$L_z =$	461.1 ft
Q =	0.84
$I_z =$	0.21
G =	0.84

Flexible structure if natural frequency	< 1 Hz (T > 1 second).
If building h/B>4 then may be flexible	and should be investigated.
h/B = 0.18	Rigid structure (low rise bldg)

## G = 0.85 Using rigid structure default

Flexible or Dyna	amically Ser	nsitive S	tructure		
Natural Frequency $(\eta_1) =$	0.7 Hz				
Damping ratio (β) = /b =	0.01 0.660				
/α = Vz =	0.156 104.5				
N <sub>1</sub> =	3.09				
R <sub>n</sub> =	0.069				
R <sub>h</sub> =	0.534	η =	1.131	h =	36.7 ft
R <sub>B</sub> =	0.149	η =	6.163		
$R_L =$	0.038	η =	25.789		
g <sub>R</sub> =	4.104				
R =	0.547				
Gf =	0.960				

Company Address City, State Phone Example 3.3 & 4.1 Example 3.3 & 4.1

JOB NO.	SHEET NO.	
CALCULATED BY	DATE	
CHECKED BY	DATE	

### **Ground Elevation Factor (Ke)**

Grd level above sea level =	0 ft	Ke =	1.0000
Constant =	0.00256		
0.00256Ke =	0.00256		

#### **Enclosure Classification**

Test for Enclosed Building:	Ao < 0.01Ag or 4 sf, whichever is smaller
Test for Open Building:	All walls are at least 80% open. Ao ≥  0.8Ag

Test for Partially Enclosed Building: Predominately open on one side only

	Input			Test	
Ao	500.0	sf	Ao ≥ 1.1Aoi	NO	
Ag Aoi	600.0	sf	Ao > 4sf or 0.01Ag	YES	
Aoi	1000.0	sf	Aoi / Agi ≤ 0.20	YES	Building is NOT
Agi	10000.0	sf			Partially Enclosed

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

Ao ≥ 1.1Aoi

Ao > smaller of 4sf or 0.01 Ag Aoi / Agi  $\leq 0.20$ 

Where:

Ao = the total area of openings in a wall that receives positive external pressure.

Ag = the gross area of that wall in which Ao is identified.

Aoi = the sum of the areas of openings in the building envelope (walls and roof) not including Ao.

Agi = the sum of the gross surface areas of the building envelope (walls and roof) not including Ag.

#### Test for Partially Open Building:

A building that does not qualify as open, enclosed or partially enclosed. (This type building will have same wind pressures as an enclosed building.)

### Reduction Factor for large volume partially enclosed buildings (Ri) :

If the partially enclosed building contains a single room that is unpartitioned, the internal pressure coefficient may be multiplied by the reduction factor Ri.

Total area of all wall & roof openings (Aog):		- SF
Unpartitioned internal volume (Vi):		- CF
	Ri =	1.00

Company	Example 3.3 JOB TITLE Exar	mple 3.3 & 4.1
Address		
City, State	JOB NO.	SHEET NO.
Phone	CALCULATED BY	DATE
	CHECKED BY	DATE

## Wind Loads - MWFRS all h (Except for Open Buildings)

Base pressure (qh) = (Kd qh) = Roof Angle (θ) = Roof trib Wind normal to ridge =(h/2)*L:	34.6 psf <b>29.4 psf</b> 18.4 deg utary area: 4588 sf	Kh = Bldg dim parallel to ridge = Bldg dim normal to ridge = h = ridge ht =	1.022 250.0 ft 200.0 ft 36.7 ft 53.4 ft	GCpi = G = qi = qh	+/-0.18 0.85
Wind parallel to ridge = $(h/2)$ *L:	3670 sf		00111		

#### Ultimate Wind Surface Pressures (psf)

	Wind Normal to Ridge				Wind Parallel to Ridge				
	L/B =	0.80	h/L =	0.18		L/B =	L/B = 1.25		0.15
Surface	Ср	$q_h GC_p$	w/+q <sub>i</sub> GC <sub>pi</sub>	w/-q <sub>h</sub> GCpi	Dist.*	Ср	$q_h GC_p$	w/ +q <sub>i</sub> GC <sub>pi</sub>	w/ -q <sub>h</sub> GC <sub>pi</sub>
Windward Wall (WW)	0.80	20.0	see tab	le below		0.80	20.0	seet	able below
Leeward Wall (LW)	-0.50	-12.5	-17.8	-7.2		-0.45	-11.2	-16.5	-6.0
Side Wall (SW)	-0.70	-17.5	-22.8	-12.2		-0.70	-17.5	-22.8	-12.2
Leeward Roof (LR)	-0.57	-14.2	-19.5	-8.9		Inc	cluded in w	indward roof	
Neg Windward Roof pressure	-0.36	-9.1	-14.4	-3.8	0 to h/2*	-0.90	-22.5	-27.8	-17.2
Pos/min Windward Roof press.	0.14	3.4	-1.9	8.7	h/2 to h*	-0.90	-22.5	-27.8	-17.2
					h to 2h*	-0.50	-12.5	-17.8	-7.2
					> 2h*	-0.30	-7.5	-12.8	-2.2
					Min press.	-0.18	-4.5	-9.8	0.8

\*Horizontal distance from windward edge

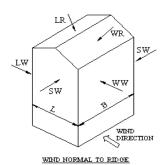
#### Windward roof overhangs: 20.0 psf (upward : add to qhGCp windward roof pressure)

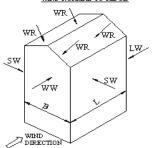
#### Parapet

Z	Kz	Kzt	Kdqp (psf)
0.0 ft	0.851	1.00	0.0
Windwa	ard parapet:	0.0 pst	(GCpn = +1.5)
Leewa	ard parapet:	0.0 psf	(GCpn = -1.0)

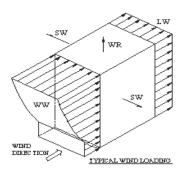
#### Windward Wall Pressures at "z" (psf)

	Windwar		Combined WW + LW					
				V	Vindward Wa		Wind Normal	Wind Parallel
	z	Kz	Kzt	$q_z GC_p$	w/+q_iGC_{pi}	w/-q_hGC_{pi}	to Ridge	to Ridge
_	0 to 15'	0.85	1.00	16.7	11.4	21.9	29.2	27.9
	20.0 ft	0.90	1.00	17.7	12.4	23.0	30.2	28.9
	25.0 ft	0.94	1.00	18.5	13.2	23.8	31.0	29.7
	30.0 ft	0.98	1.00	19.2	13.9	24.5	31.7	30.4
h=	36.7 ft	1.02	1.00	20.0	14.7	25.3	32.5	31.2
ridge =	53.4 ft	1.10	1.00	21.6	16.3	26.9	34.1	32.8





WIND PARALLEL TO RIDGE



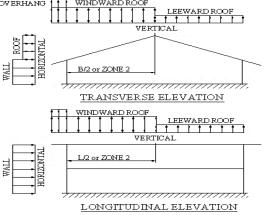
		(	Company Address			JOB TITLE	Example 3	.3 & 4.1		
			City, State Phone			JOB NO. CALCULATED BY CHECKED BY			SHEET NO. DATE DATE	
Wind L	.oads - M	WFRS h	l <b>≤60'</b> (Low-1	ise Buildi	ngs) except f	or open buildings				
I	Base pressi	ure (qh) = (Kd qh) = GCpi =	34.6 psf <b>29.4 psf</b> +/-0.18		Kz = Kh =	1.022	Edge Strip End Zone Zone 2 len	(2a) =	14.7 ft 29.4 ft 91.8 ft	
		Wind Pr	essure Co	pefficien	ts					
		C	ASE A		-			CASE B		
	Surface	GCpf	θ = 18.4 deg w/-GCpi	w/+GCpi			GCpf	w/-GCpi	w/+GCpi	
	1	0.52	0.70	0.34			-0.45	-0.27	-0.63	
	2	-0.69	-0.51	-0.87			-0.69	-0.51	-0.87	
	3	-0.47	-0.29	-0.65			-0.37	-0.19	-0.55	
	4 5	-0.42	-0.24	-0.60			-0.45 0.40	-0.27 0.58	-0.63 0.22	
	6						-0.29	-0.11	-0.47	
	1E	0.78	0.96	0.60			-0.48	-0.30	-0.66	
	2E	-1.07	-0.89	-1.25			-1.07	-0.89	-1.25	
	3E 4E	-0.67 -0.62	-0.49 -0.44	-0.85 -0.80			-0.53 -0.48	-0.35 -0.30	-0.71 -0.66	
	4E 5E	-0.02	-0.44	-0.00			-0.48	-0.30 0.79	-0.66	
	6E						-0.43	-0.25	-0.61	
		Ultimate	Wind Su	rface Pr	essures (p	osf)				
	1		20.5	9.9				-7.9	-18.5	
	2		-15.0	-25.6				-15.0	-25.6	
	3		-8.5	-19.1				-5.6	-16.2	
	4 5		-6.9	-17.5				-7.9 17.1	-18.5 6.5	
	6							-3.2	-13.8	
	1E		28.2	17.6				-8.8	-19.4	
	2E		-26.2	-36.8				-26.2	-36.8	
	3E 4E		-14.5 -12.9	-25.1 -23.5				-10.3 -8.8	-20.9 -19.4	
	4L 5E		-12.5	-20.0				23.2	12.6	
	6E							-7.4	-17.9	
	Parapet									
N N	Windward p		0.0		pn = +1.5)	Windward		20.0	nof (university)	
	Leeward p	arapet =	0.0	psi (GC	on = -1.0)	0\	verhangs =	20.6	psf (upward) windward ro	
		<b></b> .			0	WINDWARD OVERHANG	WINDWAR	<u> ಇಂಂಕ</u>	winuwaru 10	or pressure
Horizonta		-	aphragm Pr		<u>pst)</u>				LEEWARD ROOF	
	Transvers		n (normal to			<u>ل</u> ا ب <del>ہ ہ</del> ر ا		VERTIC.		
		Roof	27.4 -6.5	psi psf **		ROOF NTAL				
	End Zo	ne: Wall	41.1	psf		┌─┶╾┥ᢓ	B/2 or ZON	IE 2		
		Roof	-11.7	psf **		WALL	-	24	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<del>,</del>

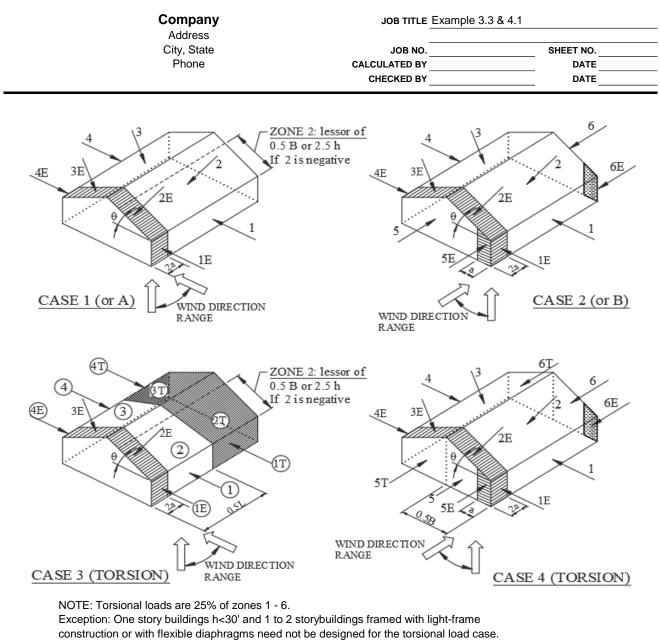
#### Longitudinal direction (parallel to L)

Interior Zone: Wall 20.3 psf End Zone: Wall 30.6 psf

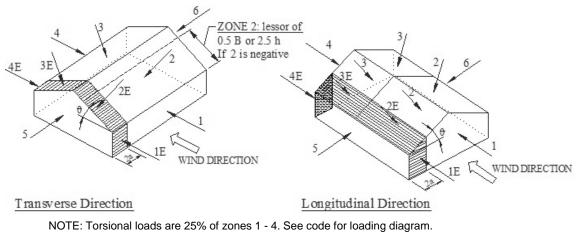
\*\* NOTE: Total horiz force shall not be less than that determined by neglecting roof forces (except for MWFRS moment frames).

The code requires the MWFRS be designed for a min ultimate force of 16 psf multiplied by the wall area plus an 8 psf force applied to the vertical projection of the roof.





# ASCE 7-98 & ASCE 7-10 (& later) - MWFRS wind pressure zones



NOTE: Torsional loads are 25% of zones 1 - 4. See code for loading diagram. Exception: One story buildings h<30' and 1 to 2 storybuildings framed with light-frame construction or with flexible diaphragms need not be designed for the torsional load case.

# ASCE 7-02 and ASCE 7-05 - MWFRS wind pressure zones